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# **Well-test flow responses of highly heterogeneous porous and fractured media**

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# *Task T3: Well test interpretation in 2D and 3D heterogeneous porous media and in DFN*

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T3.1: Our first objective is to design an interface between ODE solvers and fast sparse linear solvers. The first target libraries will be SUNDIALS [hindmarsh et al., 2005] and HYPRE [Falgout et al., 2005]. All modules will be integrated in the HYDROLAB development platform. The transient flow solver module will be made generic to porous media, fractured media and porous fractured media.

T3.2: Our second objective is to use the transient module for simulating transient flow in heterogeneous porous media (task T1).

T3.3: We will develop a module for simulating transient flow in DFN (task T2).

T3.4: We will use the supervisor of Monte-Carlo method and the deployment of simulations on grid architectures to run multiparametric simulations (task T7). The results will be stored in a **well structured database** which will be available in the free release of the platform. **The database will be used for setting up relation between drawdown signals and the medium hydraulic properties.**

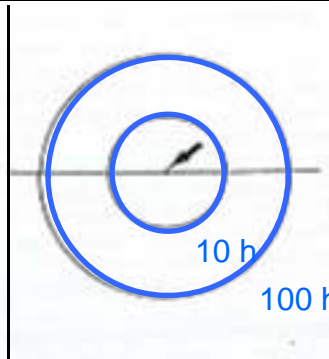
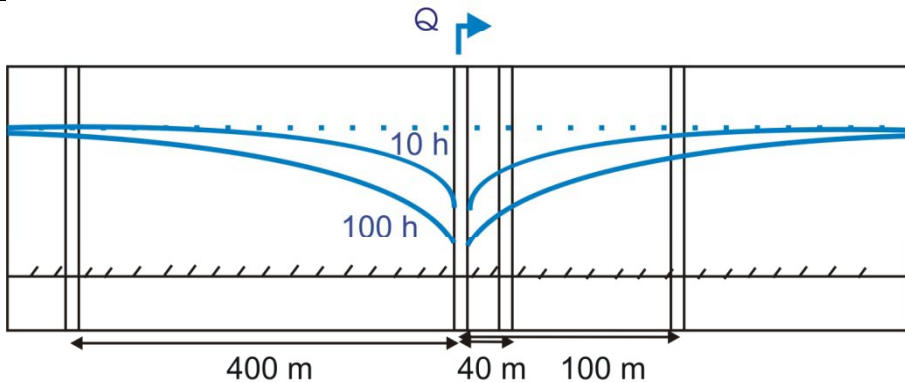
Results will be compared to signals obtained in natural fields and particularly on the site of Ploemeur (Brittany) [Le Borgne , et al., 2004]. A review of site data is given in [de Dreuzy and Davy, 2007]. This step will be undertaken in strong collaboration with the ERO H+.

# Codes

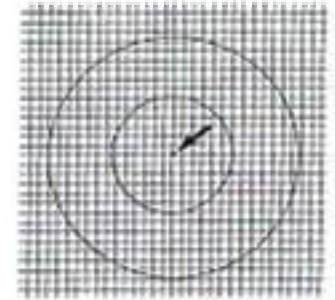
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- Modification of SUNDIALS
  - Interface to SUNDIALS
  - Integration within SUNDIALS of an interface to other linear solvers (the same as in steady state)
- Construction of the transient systems  $dH/dt=A.H$ 
  - Porous media
  - DFN
- Which applications use transient codes?
  - 2D-3D well tests
  - Hydraulic tomography
  - Fracture-Matrix

# Well-test interpretation models



$D=1$



$D=2$

- Classical flow equation  $D = 1, 2 \text{ or } 3$

$$S \frac{\partial h}{\partial t} = \frac{T}{r^{D-1}} \frac{\partial}{\partial r} \left( r^{D-1} \frac{\partial h}{\partial r} \right)$$

- Drawdown solution

$$D = 1 \quad h_r(t) \sim \sqrt{t} - 1$$

$$D = 2 \quad h_r(t) \sim \ln(t)$$

$$D = 2 \quad h_r(t) \sim 1 - 1/\sqrt{t}$$

- Generalized flow equation  $1 \leq D \leq 2$

$$S \frac{\partial h}{\partial t} = \frac{T}{r^{D-1}} \frac{\partial}{\partial r} \left( r^{D-1-(d_w-2)} \frac{\partial h}{\partial r} \right)$$

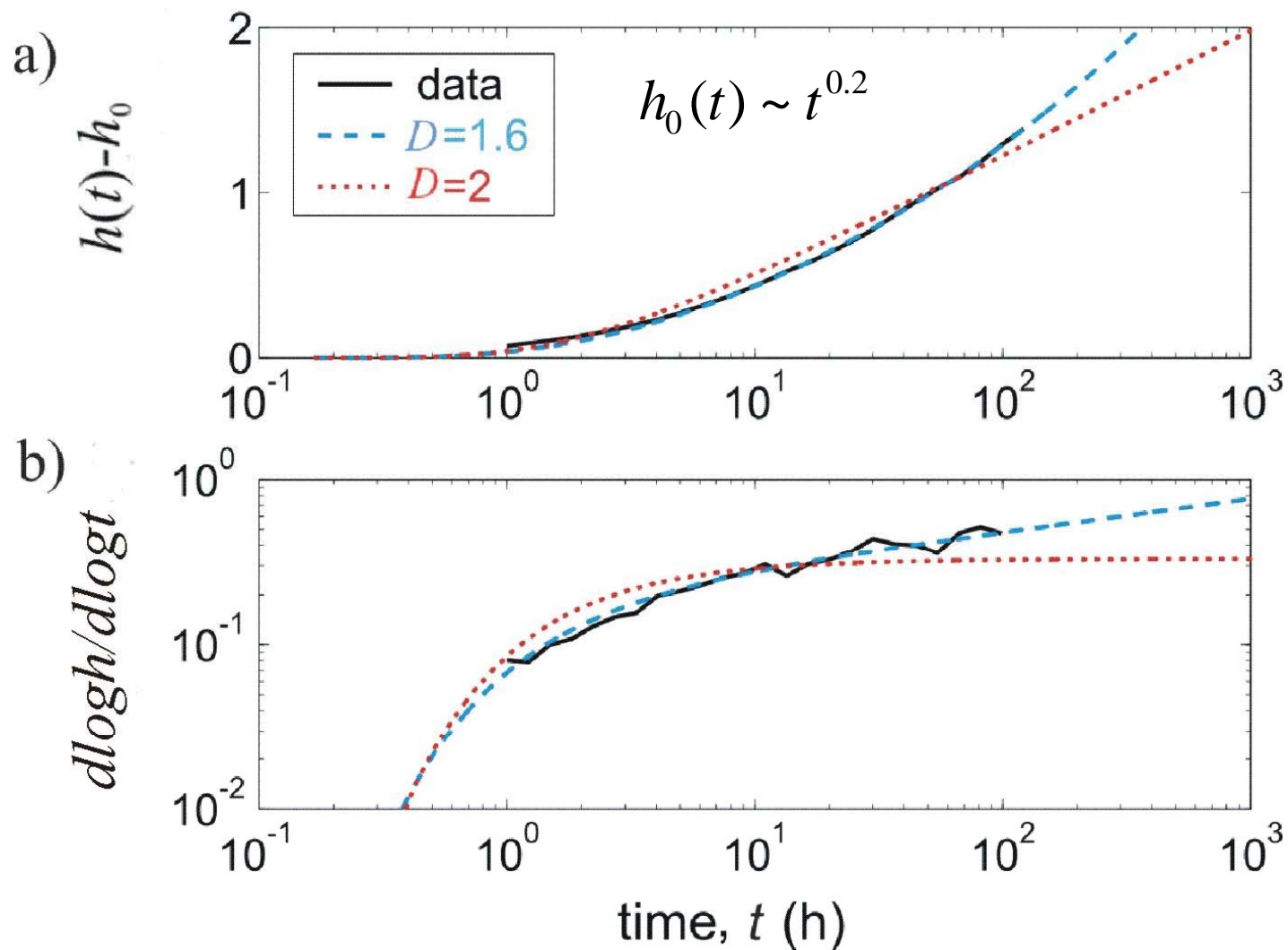
- Generalized drawdown solution

$$h_r(t) \sim \left[ \frac{t}{t_c(r)} \right]^{\left( -\frac{n}{2} \right)} \text{ with } n = \frac{2 \cdot D}{d_w}$$

$$t_c(r) \sim r^{d_w} \quad r^2(t_c) \sim t_c^{\frac{2}{d_w}}$$

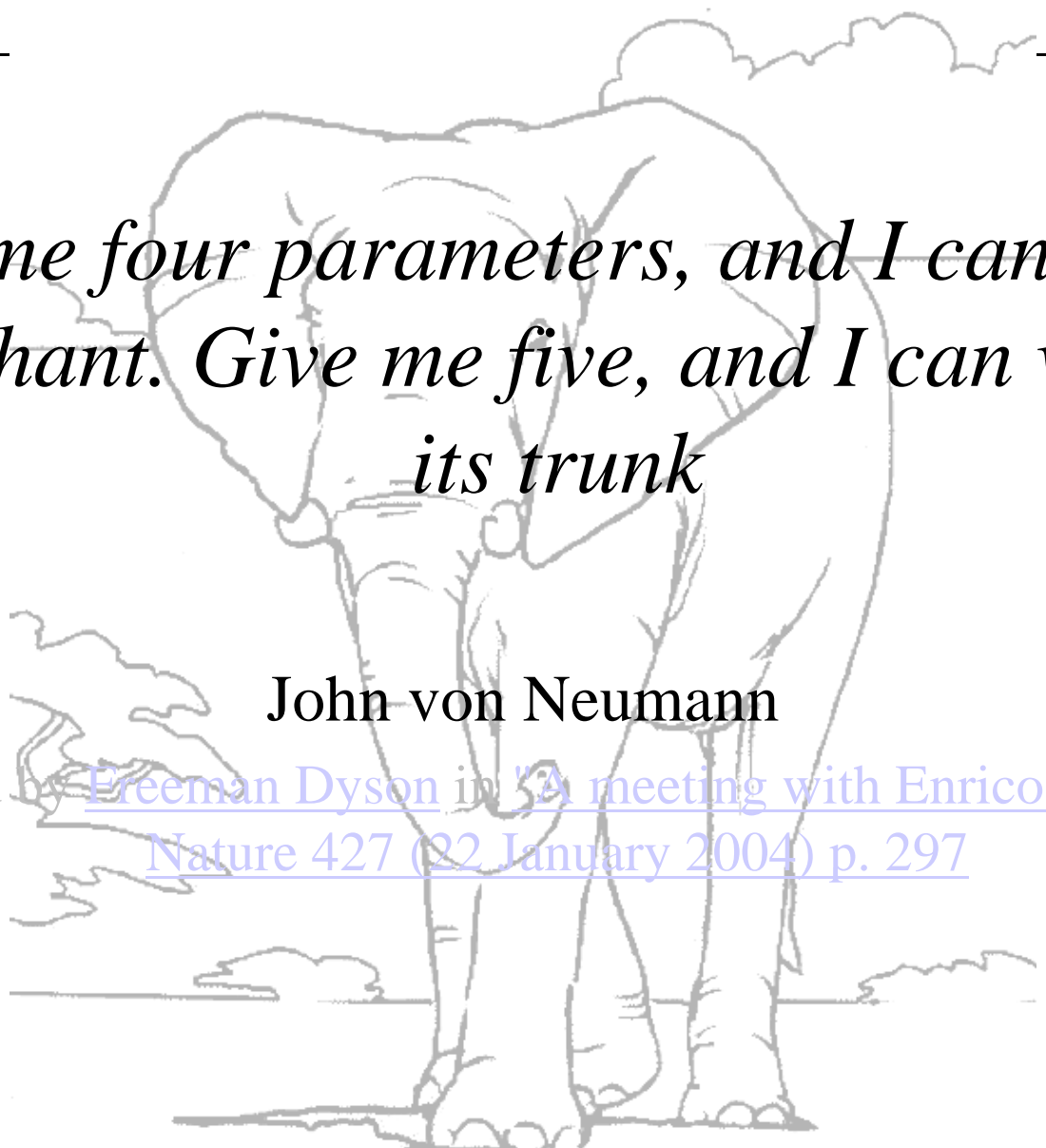
Barker [1988], Acuna and Yortsos [1996]

# Field test in a fractured aquifer (Ploemeur, France)



Le Borgne et al., *WRR*, 2004, Equivalent mean flow models for fractured aquifers:  
Insights from a pumping tests scaling interpretation

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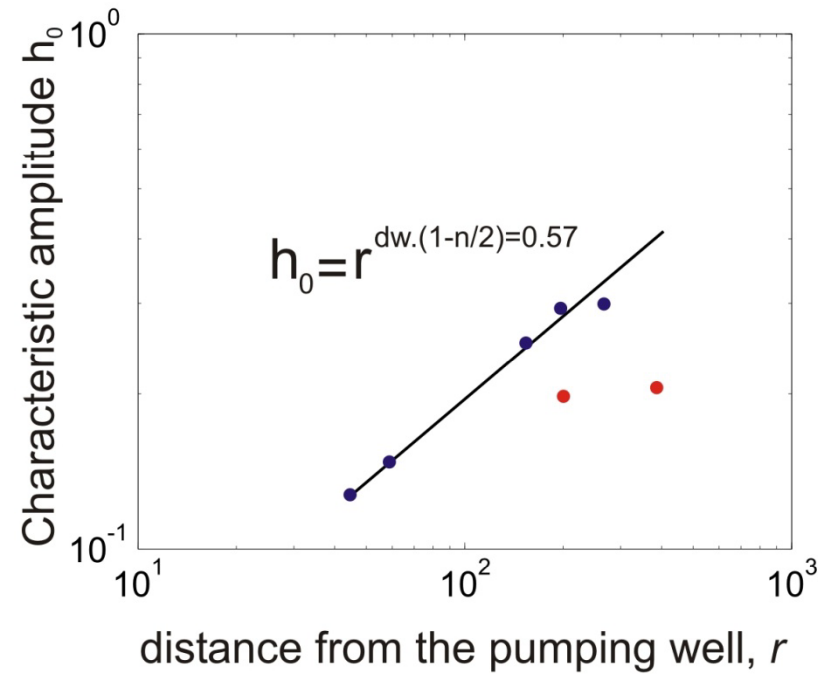
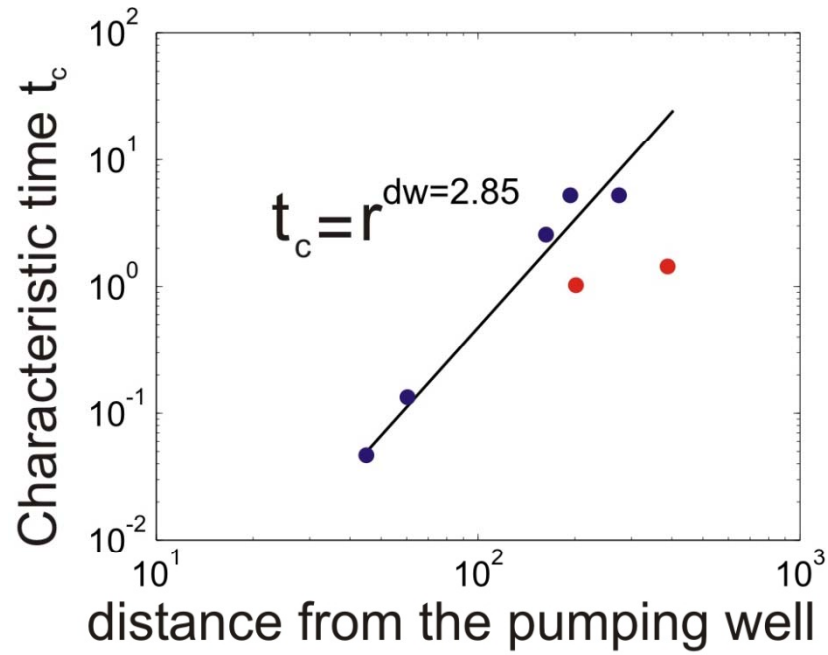


*Give me four parameters, and I can fit an  
elephant. Give me five, and I can wiggle  
its trunk*

**John von Neumann**

As quoted by [Freeman Dyson](#) in "[A meeting with Enrico Fermi](#)" in  
[Nature 427 \(22 January 2004\) p. 297](#)

# Exponent $d_w$ from the field data of Ploemeur

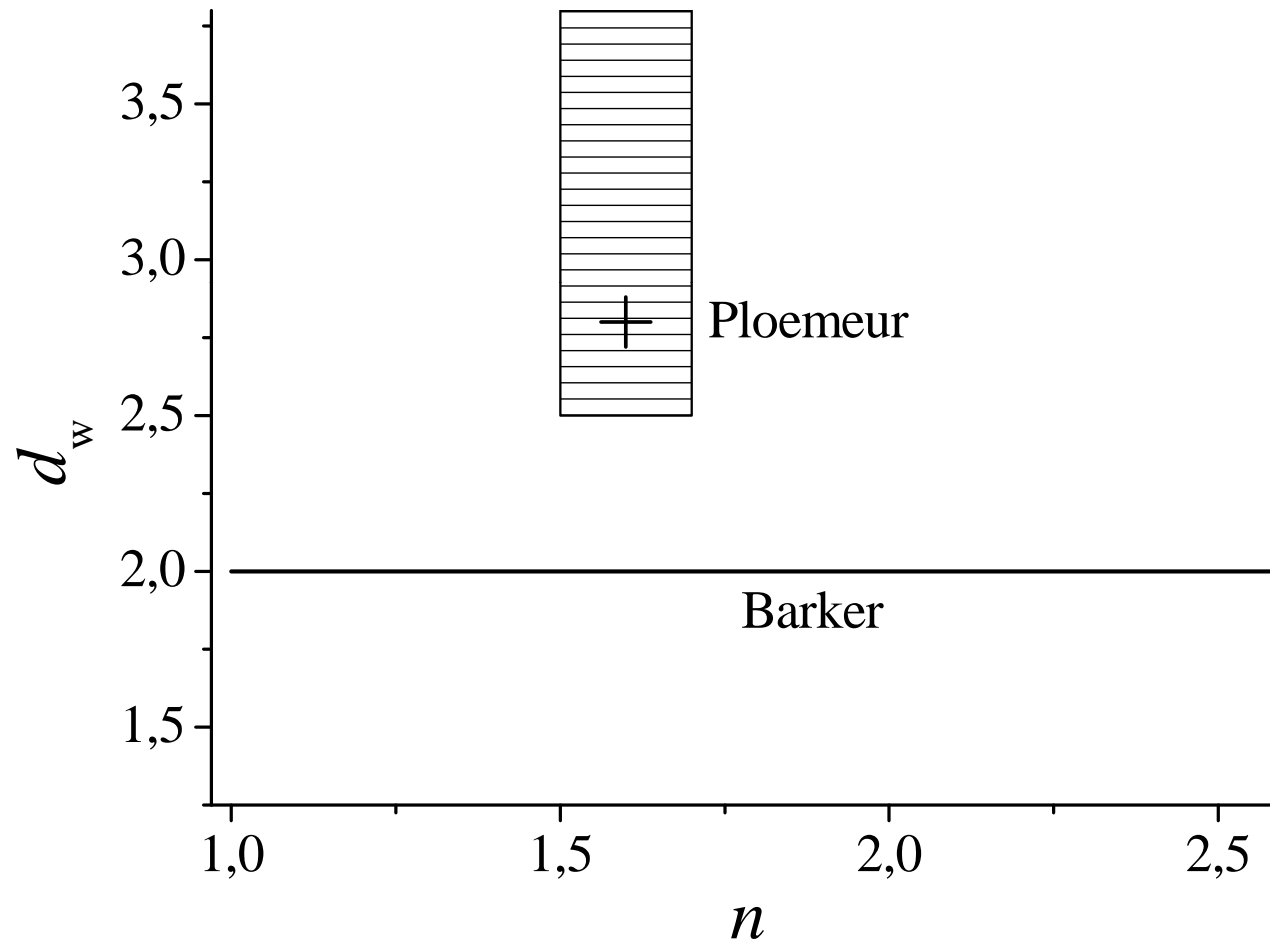


$$d_w = 2.85$$

anomalously slow drawdown diffusion

# Which permeability structure leads to non-classical drawdown response such as Ploemur's?

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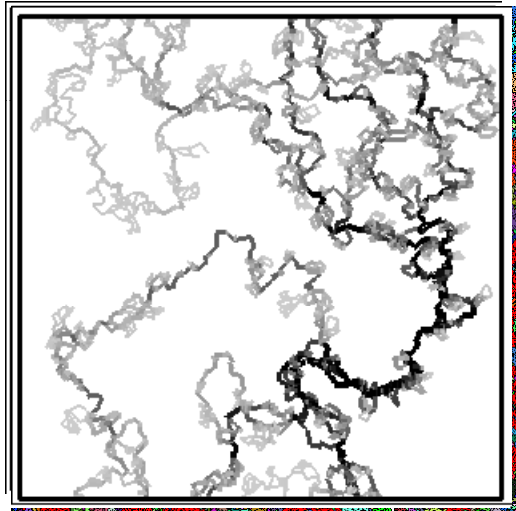




# Fractals: Percolation structures $d_f=1.86$

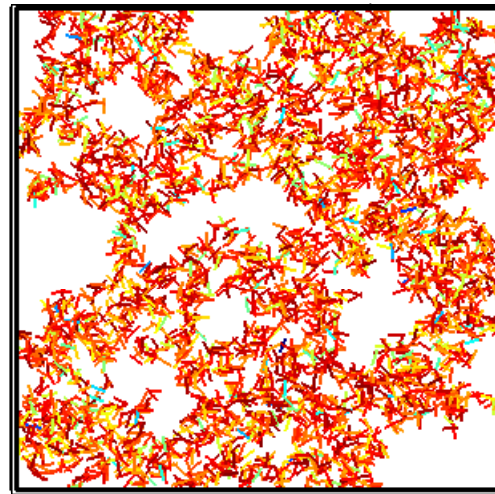
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Classical percolation



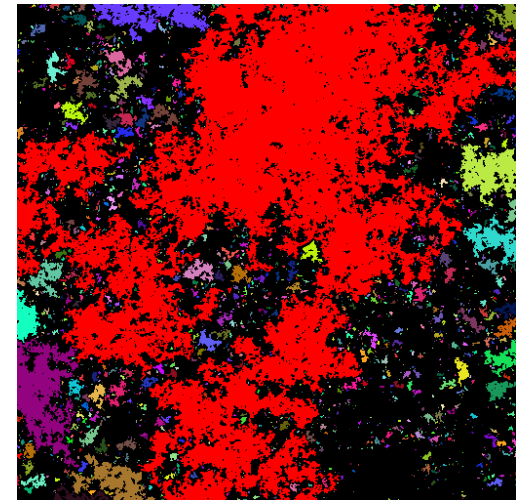
$$d_w \sim 2.9$$

Continuum percolation  
Permeability distribution



$$d_w > 2.9$$

Correlated percolation



*Makse*

$$2.3 < d_w < 2.9$$

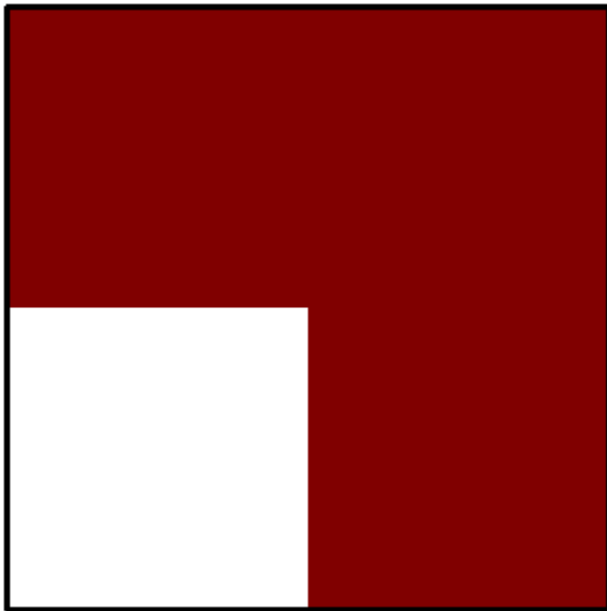
All structures have the same fractal dimension

# Fractals: Sierpinski's

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Sierpinski gasket

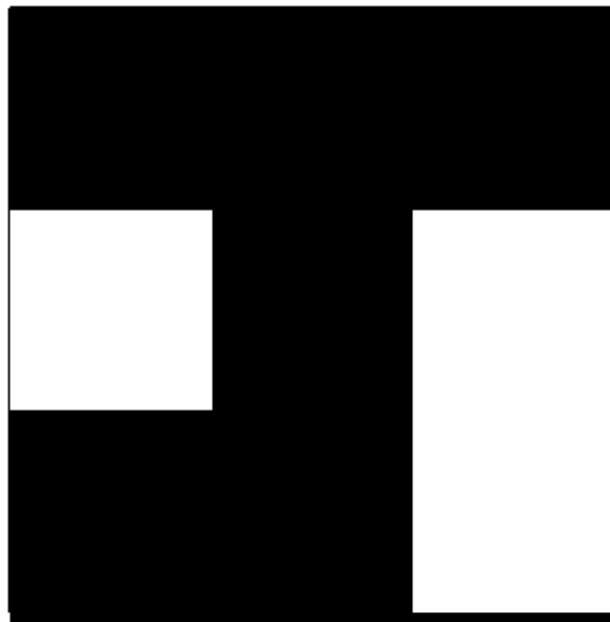
$$d_f \sim 1.6$$



$$d_w \sim 2.3$$

Generalized Sierpinski

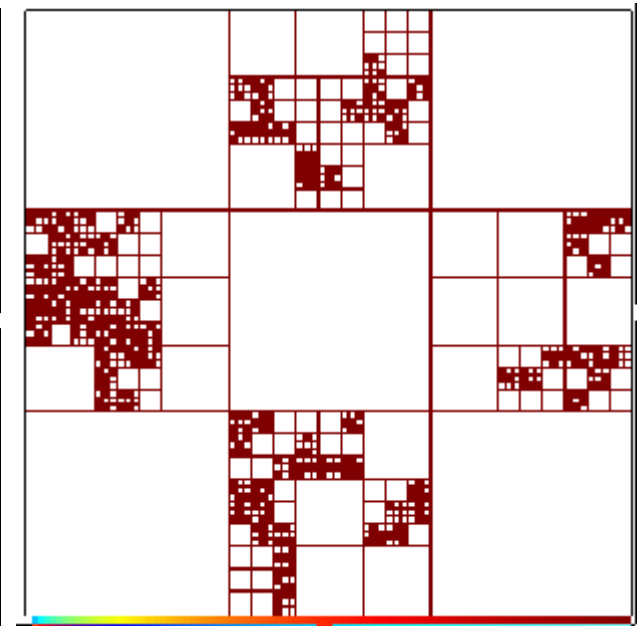
$$1.3 < d_f < 2$$



Regular multifractals with  $d_f < 2$   
become disconnected with  
increasing scale

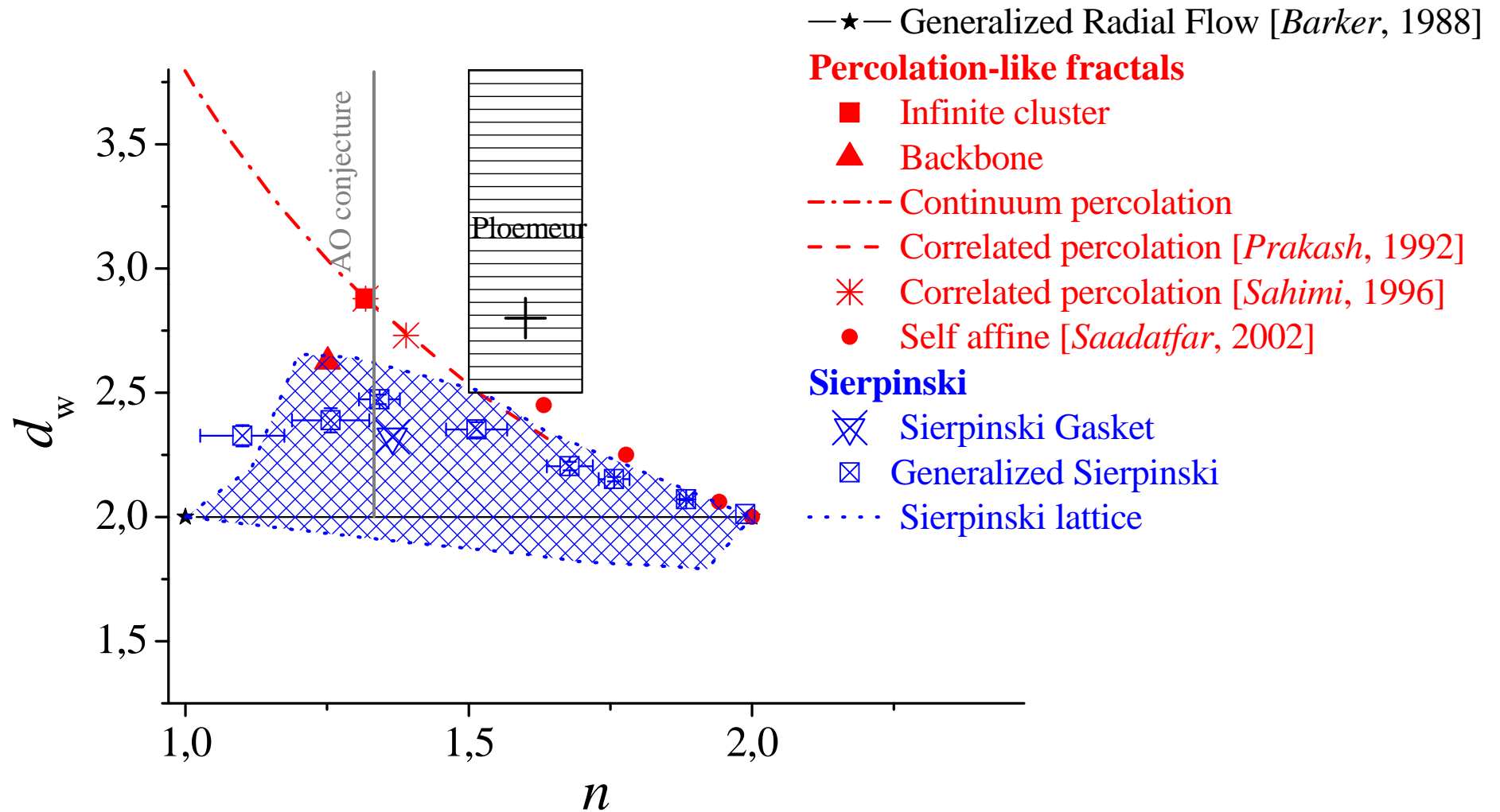
Sierpinski lattice

$$1.3 < d_f < 2$$



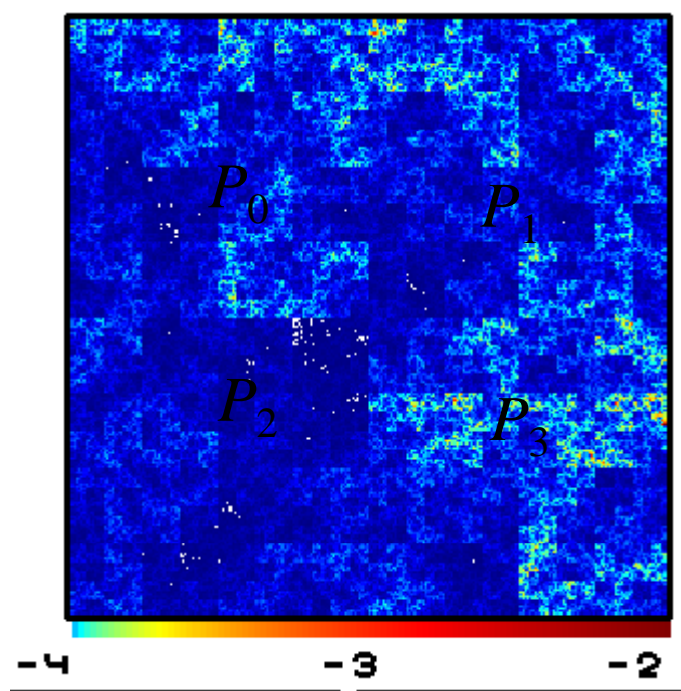
$$2 < d_w < 2.5$$

# Which permeability structure leads to non-classical drawdown response such as Ploemeur's?



# From fractal structure to long-range correlated permeability fields

## Continuous multifractals ( $d_f=2$ )

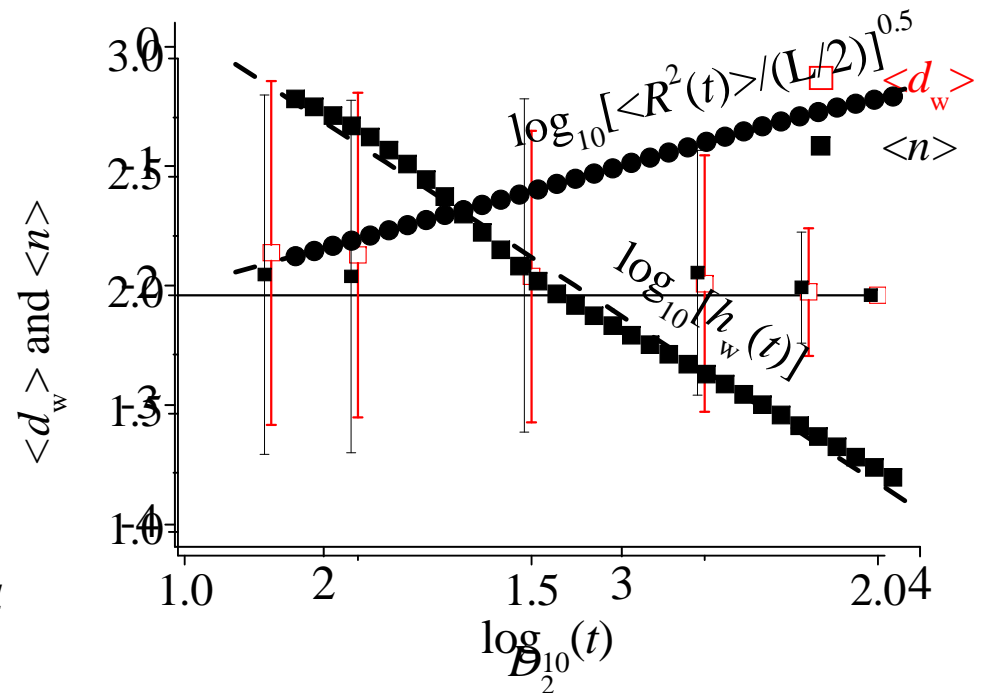


Dimensions

$P_0$	$P_1$
$P_2$	$P_3$

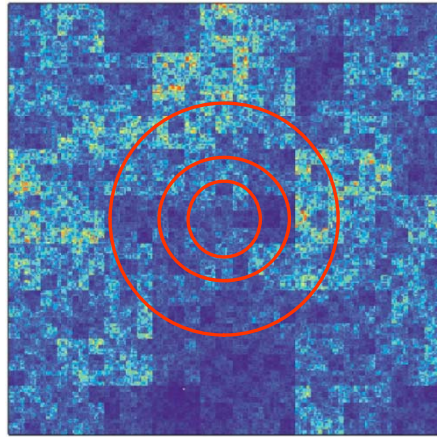
$$D_q = -\frac{\ln\left(\sum_i P_i^q\right)}{(q-1)\cdot\ln(l)}$$

$$d_f = D_0 = 2$$

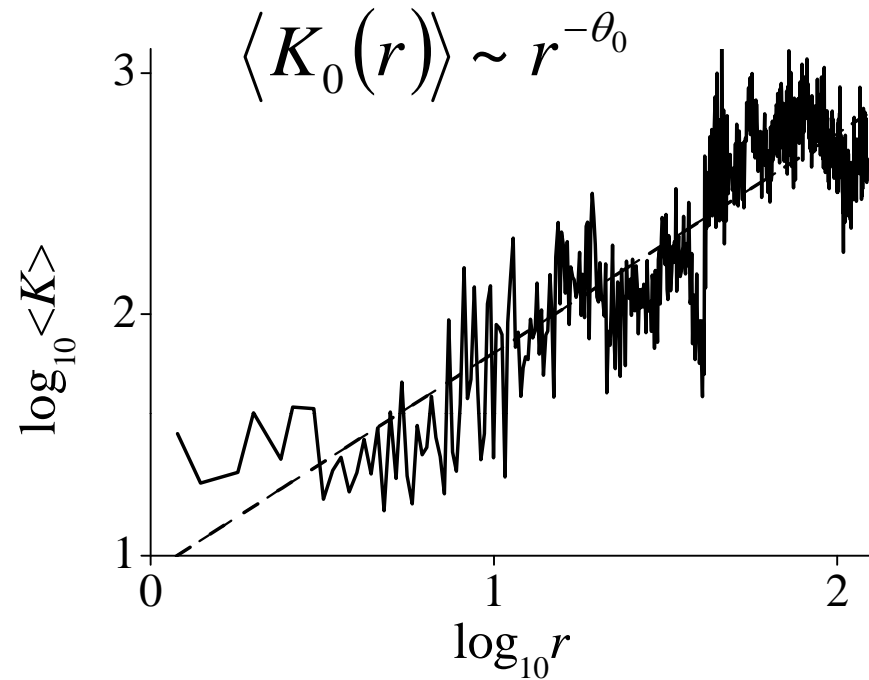


de Dreuzy et al., Physical Review E, 2004

# $d_w$ related to the permeability scaling



$\langle K_0(r) \rangle$ , the annular average

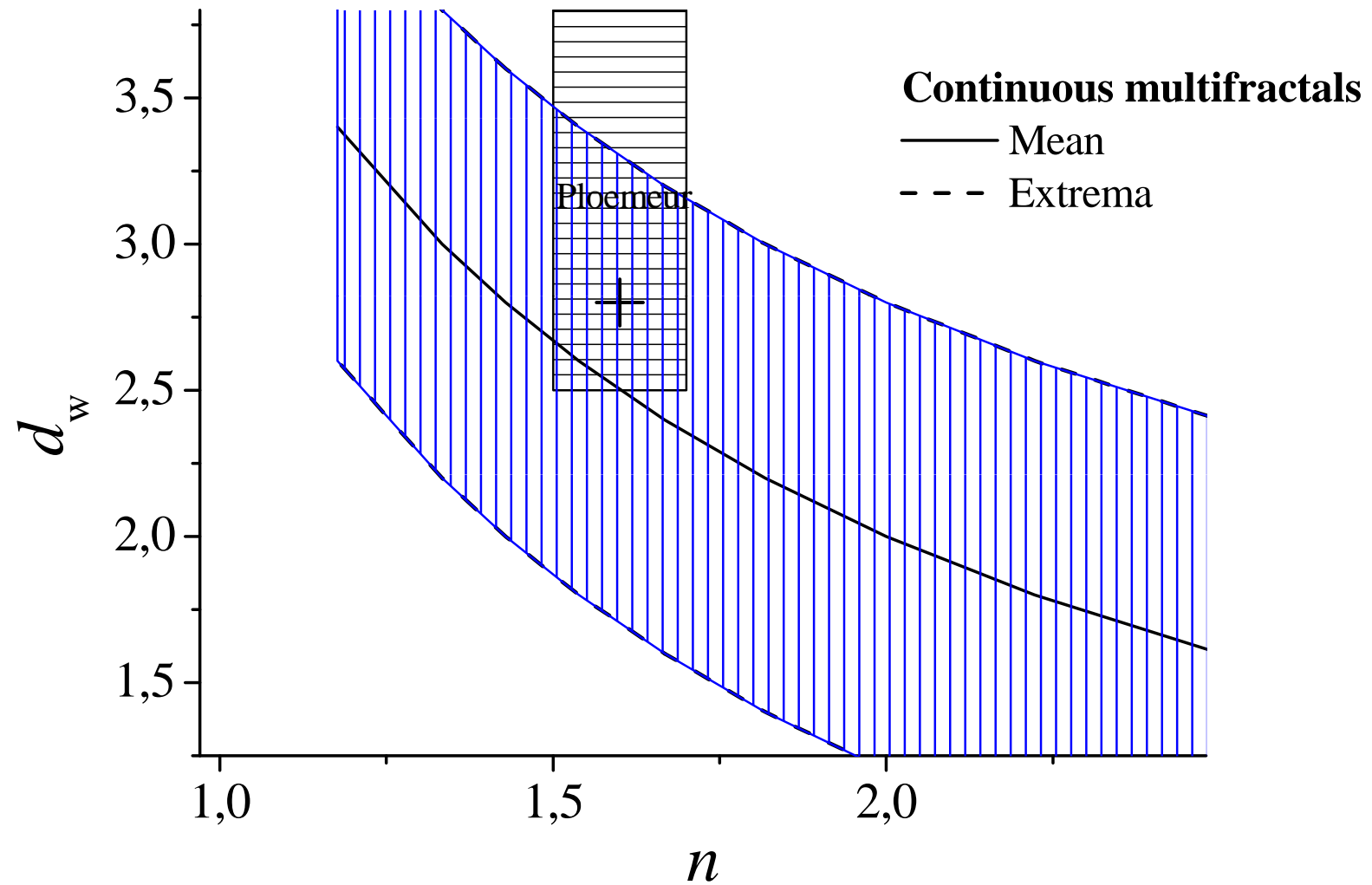


$$d_w = 2 + \theta_0 + 2 - D_2$$

- $d_w$  is given by purely geometrical exponents
- $D_2$  induces an increase of  $d_w$  by  $(2 - D_2)$  when compared to the annular case
- Through  $\theta_0$ ,  $d_w$  depends on a local property : the permeability at the well

# Which permeability structure leads to non-classical drawdown response such as Ploemeur's?

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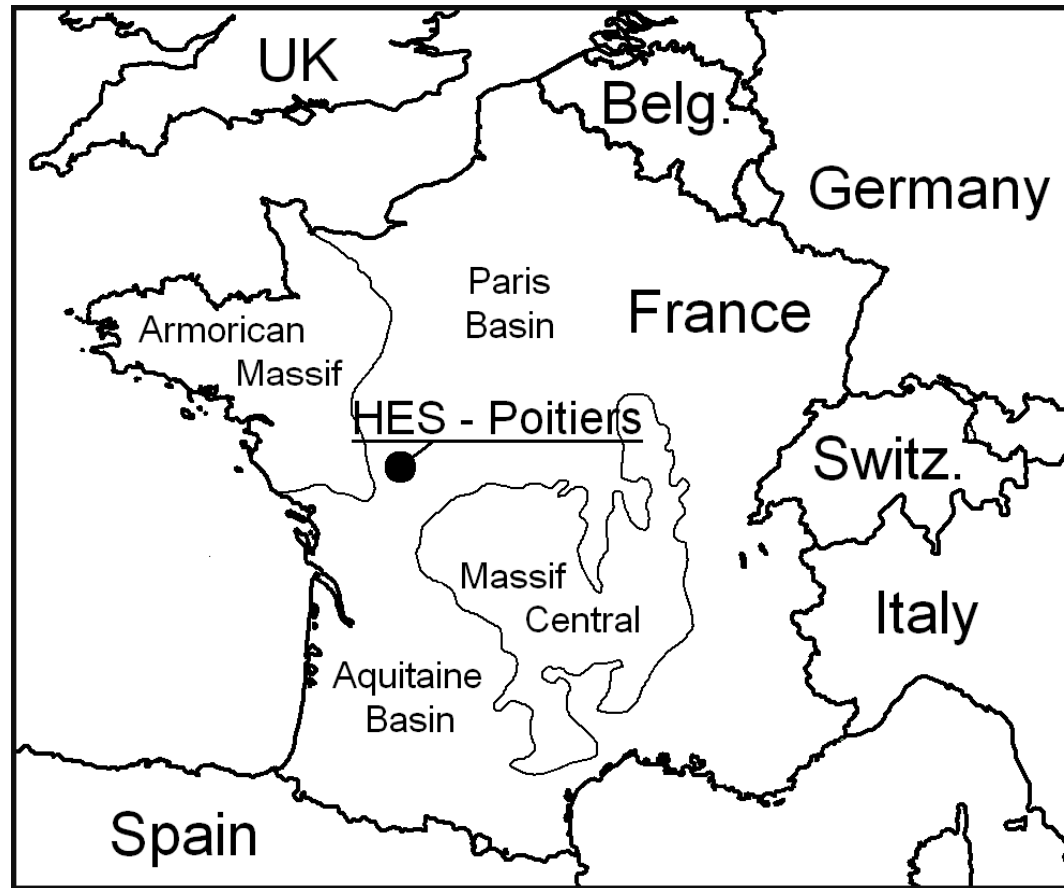


# Conclusions

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- Structure and hydraulic heterogeneity have a strong influence on transient exponents  $n$  and  $d_w$  (Percolation induces slower diffusion than Sierpinski).
- Transient exponents  $n$  and  $d_w$  depend both on **global** properties (fractal dimension) and on **local** characteristics (local permeability scaling).
- Several well tests performed from different pumping wells are necessary to find the global properties (fractal dimension, correlation dimension, ...)

# Limestone aquifer example (SEH)



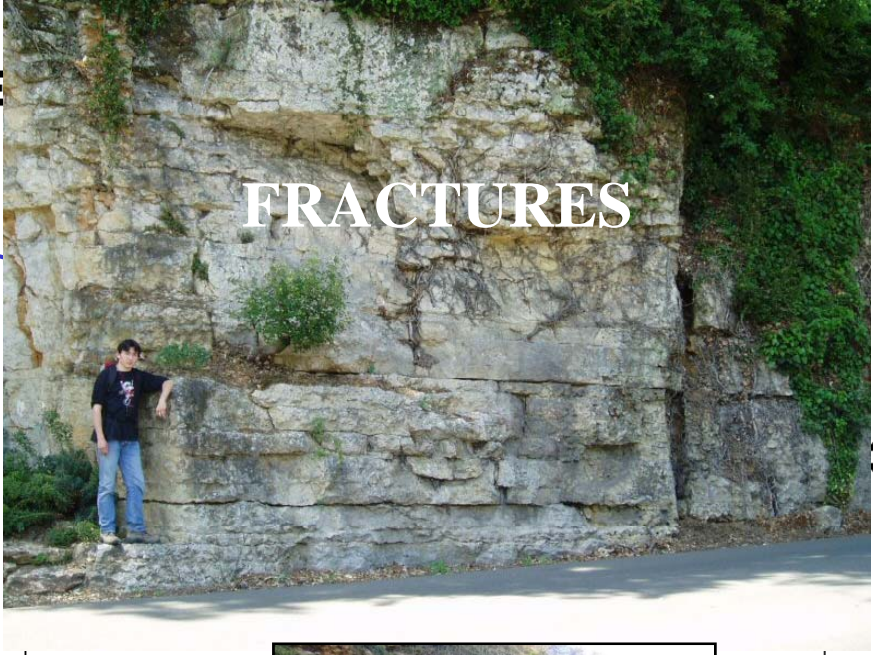
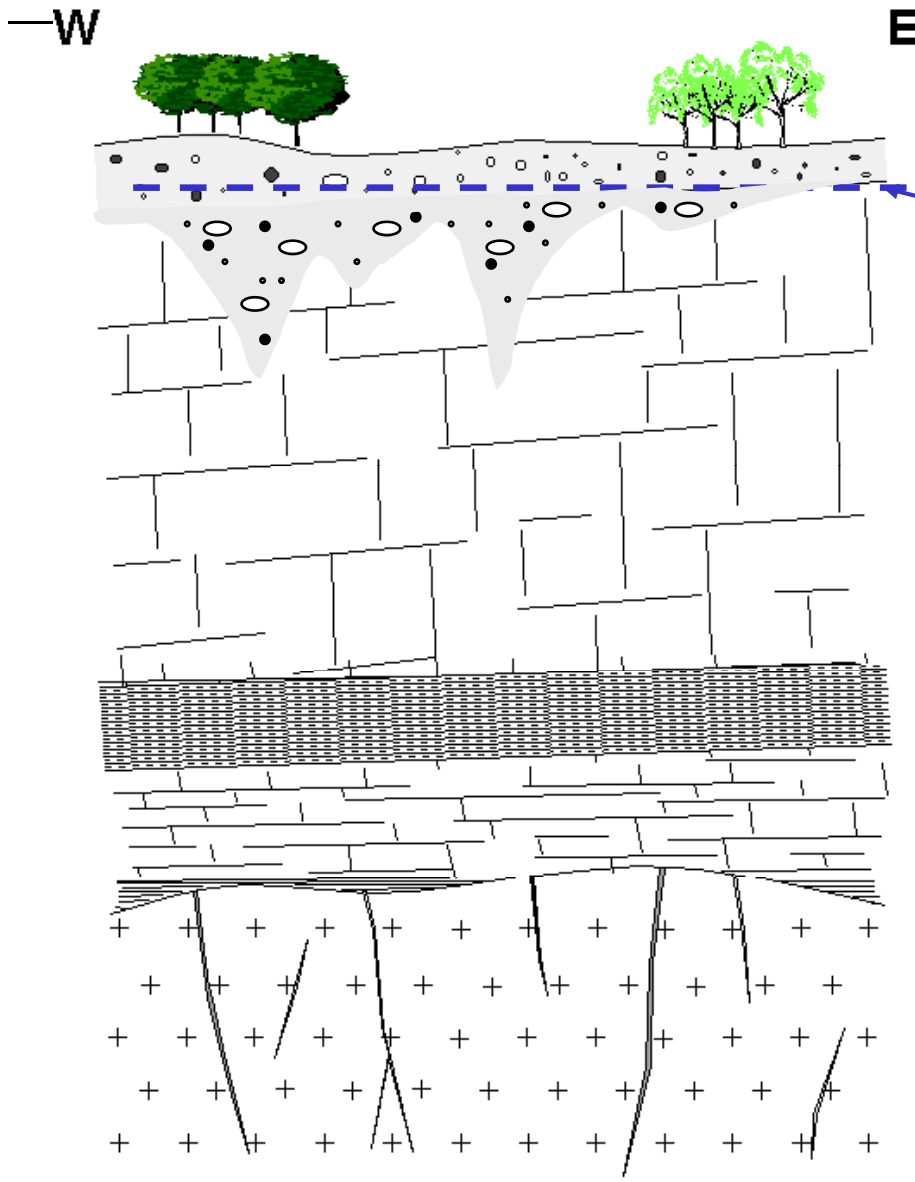
J. Bodin, G. Porel, F. Delay, University of Poitiers



# LARGE NUMBER OF WELLS

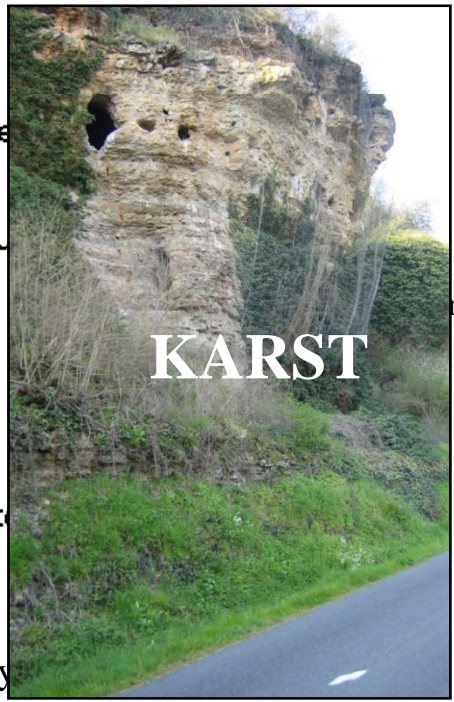


J. Bodin, G. Porel, F. Delay



30 m

Lias supérie  
Lias inférieu  
Infralias  
Granodiorite



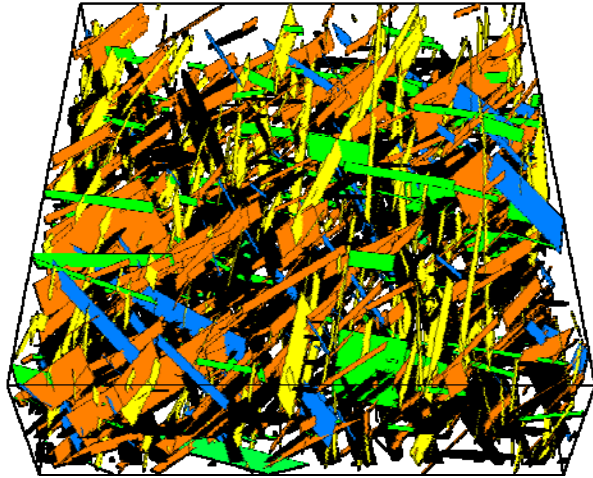
m  
m  
m

34 m

18

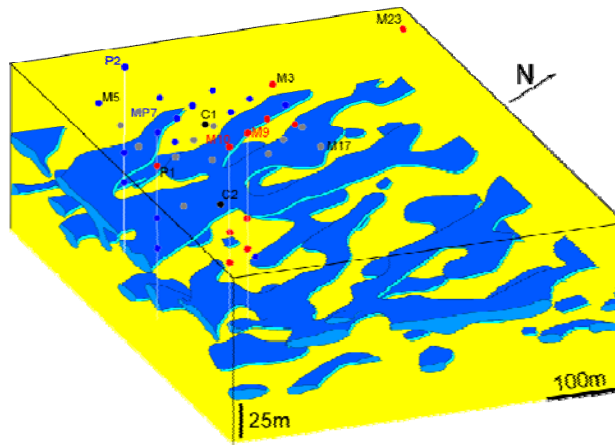
# Determination of the appropriate modeling approach?

Project: Modélisation des Aquifères Calcaires Hétérogènes (MACH) J. Bodin



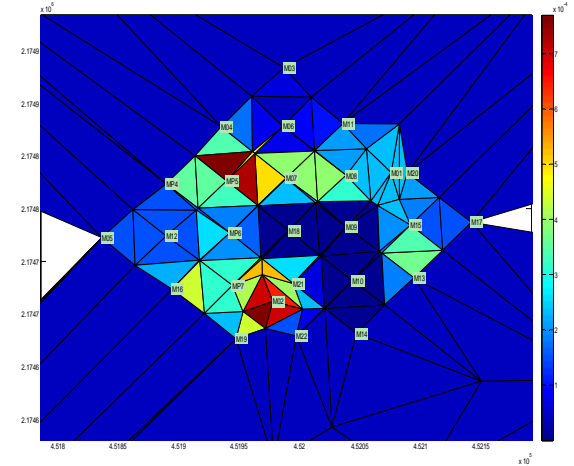
Fracture networks  
close to  
**GEOLOGY**

J. Bodin, O. Audoin



Flow channels  
close to  
**FLOW**

H. Pourpak, B. Bourbiaux, IFP



2D permeability field  
close to  
**DATA**

A. Boisson, J.-R. de Dreuzy, GR

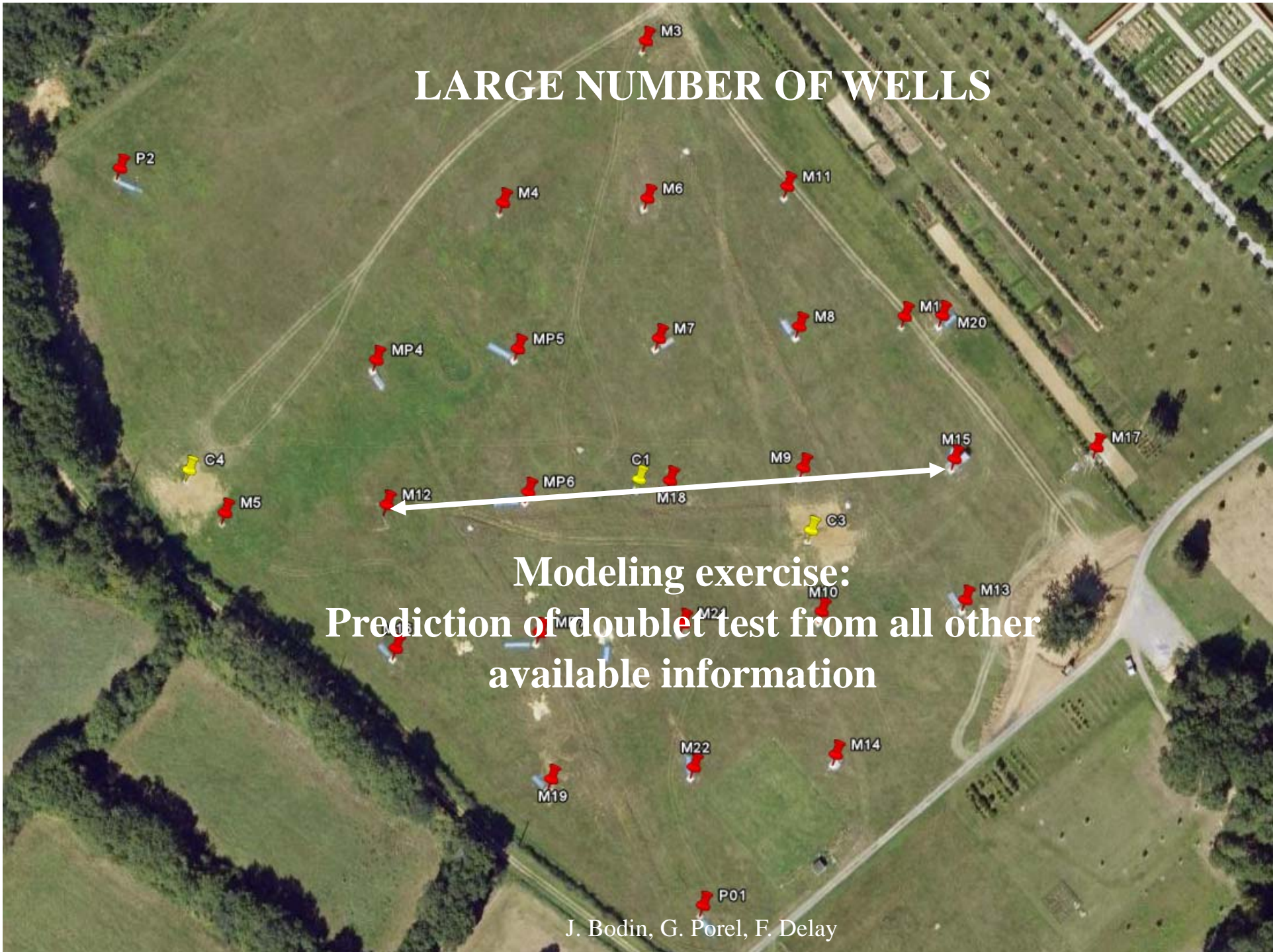
Parameters parsimony

Decreasing modeling complexity

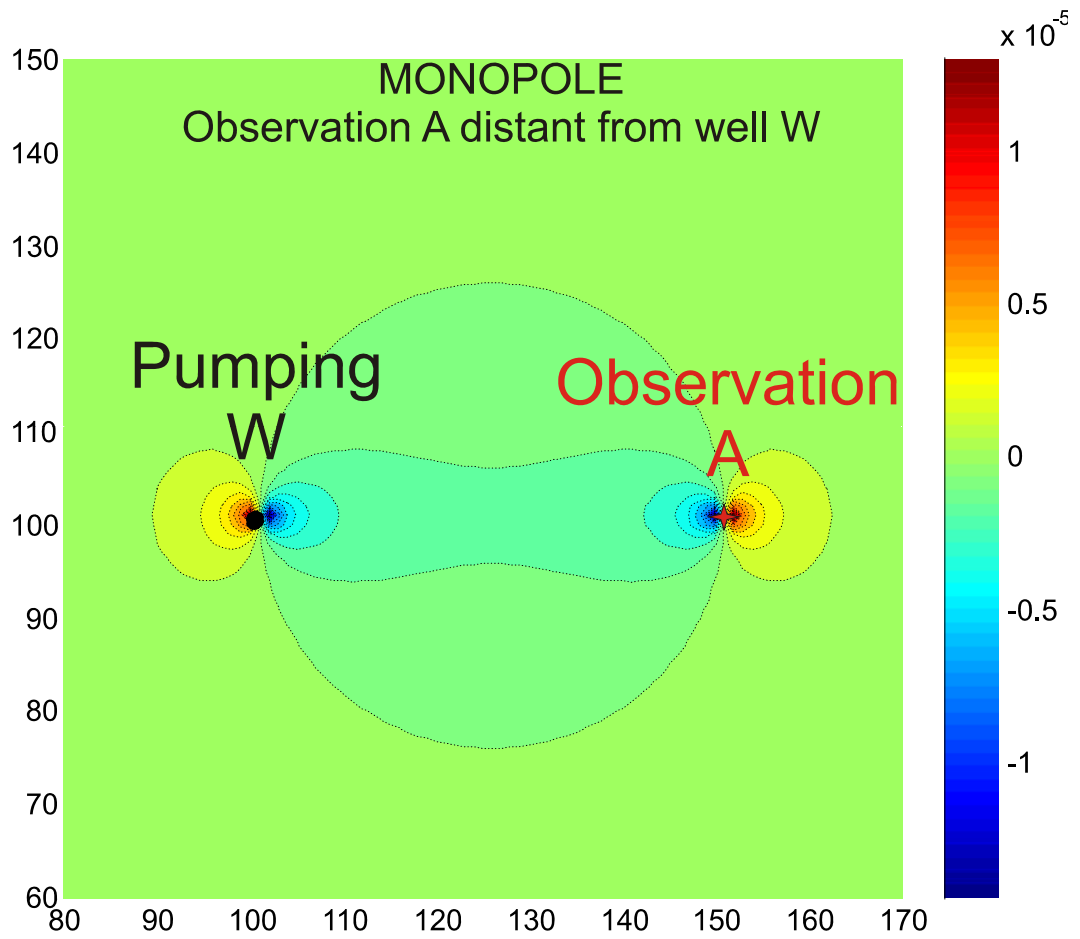
# LARGE NUMBER OF WELLS

Modeling exercise:  
Prediction of doublet test from all other  
available information

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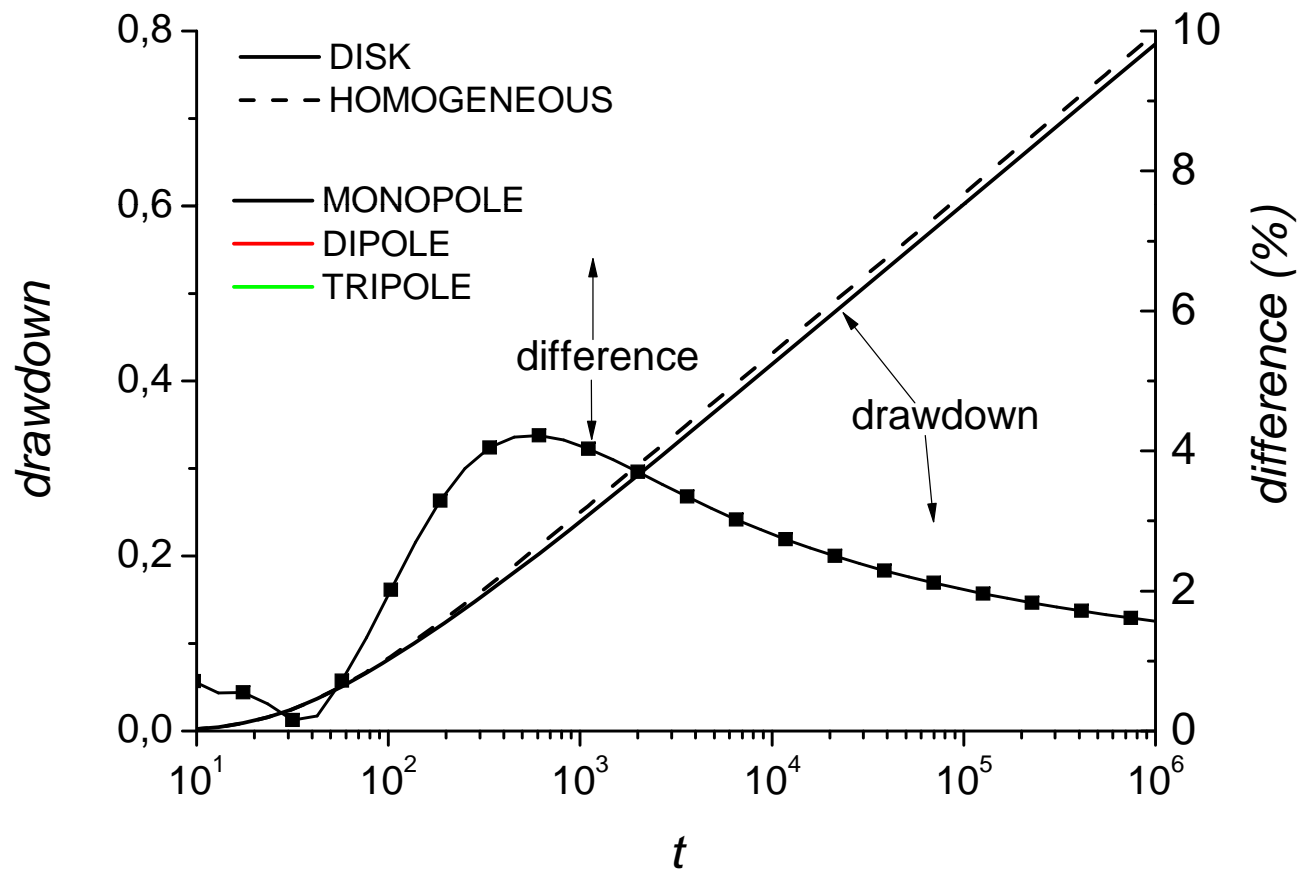


# Well tests

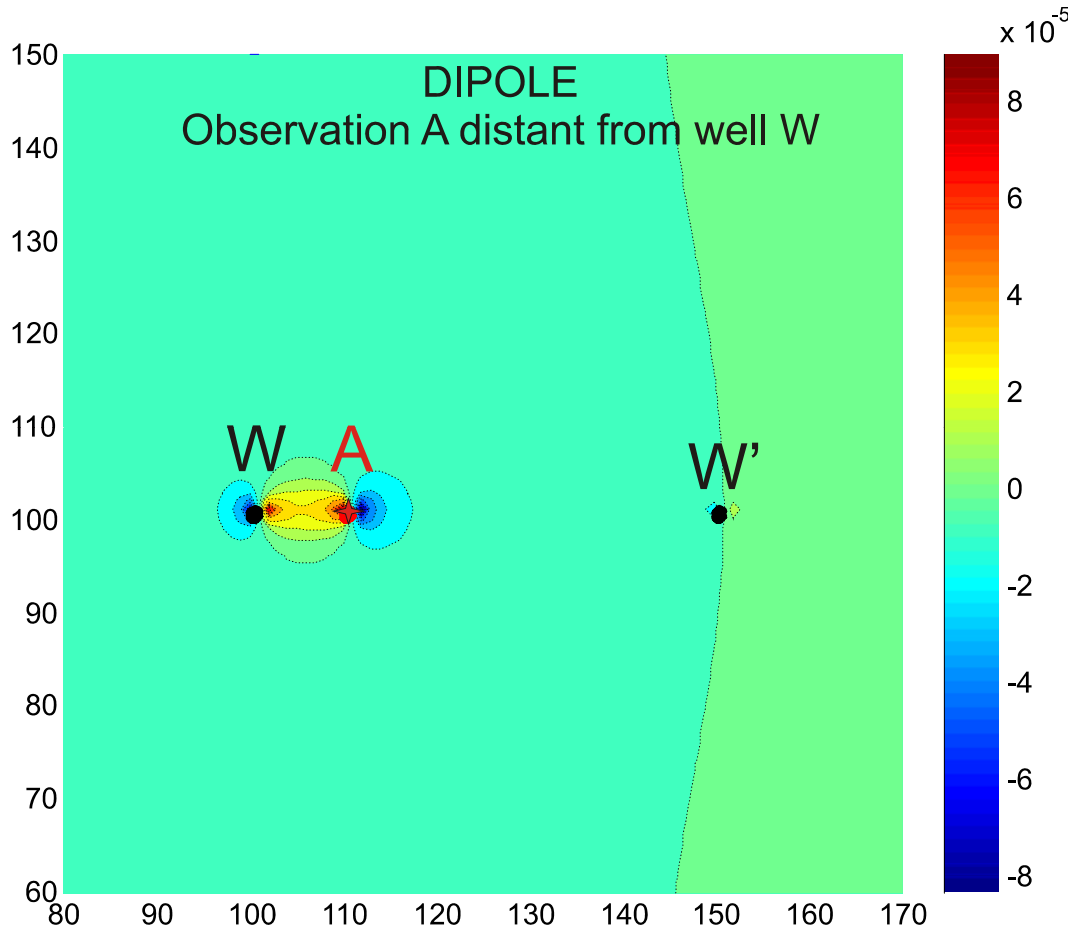


Influence localized between the well and the piezometer

# Relative drawdown

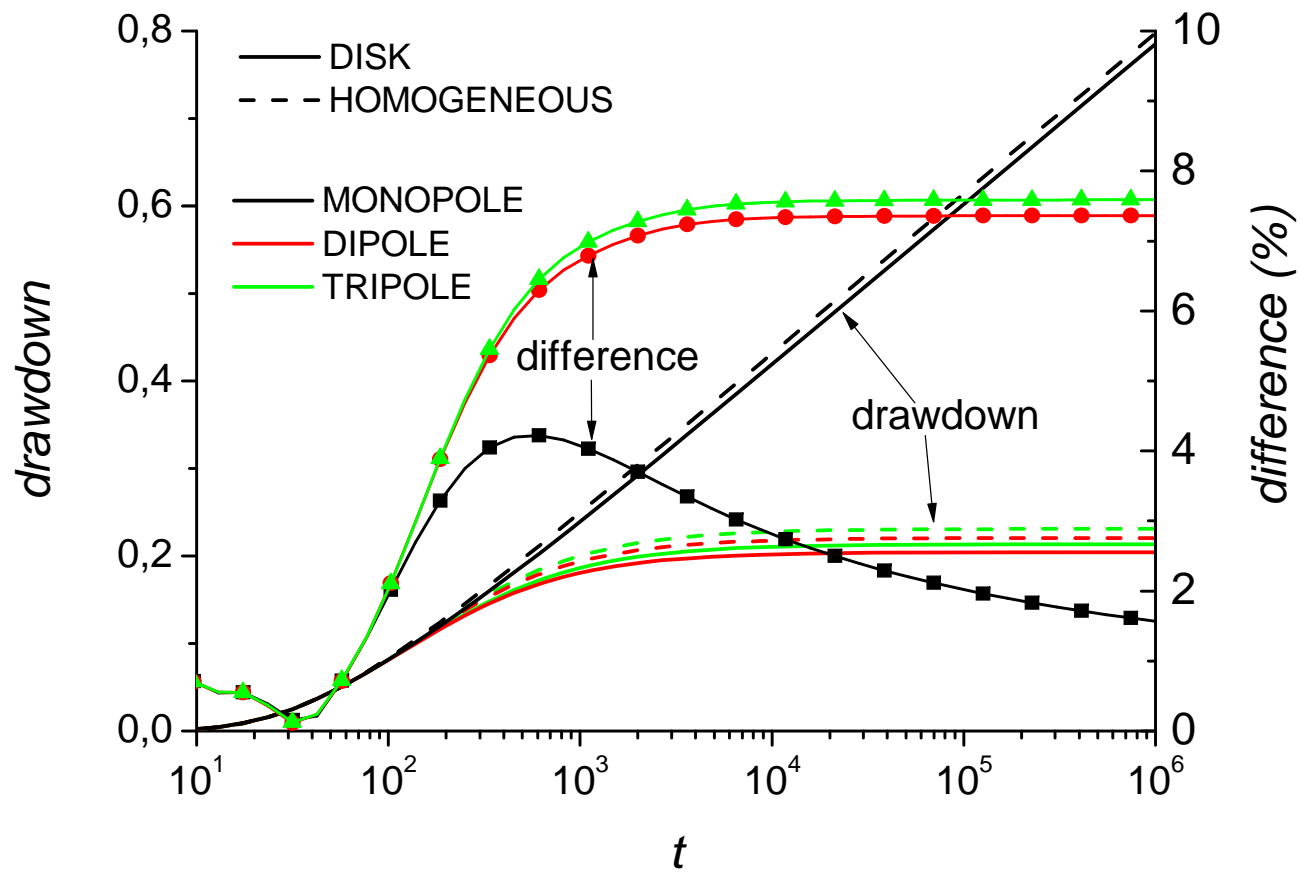


# Doublet test



Smaller influence zone  
but higher sensitivity

# Relative drawdown





# Perspectives

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- Find structures for the largest range of mean transient exponents  $n$  and  $d_{w..}$ . Are they impossible values?
- Cumulated influence of hydraulic and geometrical heterogeneities.
- Beyond models, what are the generic key structure and permeability characteristics for fixed  $n$  and  $d_{w..}$  values?
- Influence of other kind of heterogeneities (3D, fractured media)

